

# Elasticity and fracture: Is there a connection?

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## Estimates of theoretical cleavage stress

1. Orowan's criterion:<sup>12</sup> assumption of sinusoidal variation of restraining force

$$\sigma_{max} = \sqrt{\frac{E\gamma_s}{a_0}}$$

$E$ ...Young's modulus

$\gamma_s$ ...surface energy

$a_0$ ...distance between layers

2. Orowan's formula overestimates theoretical cleavage stress
3. used even in ab-initio calculations<sup>3</sup>

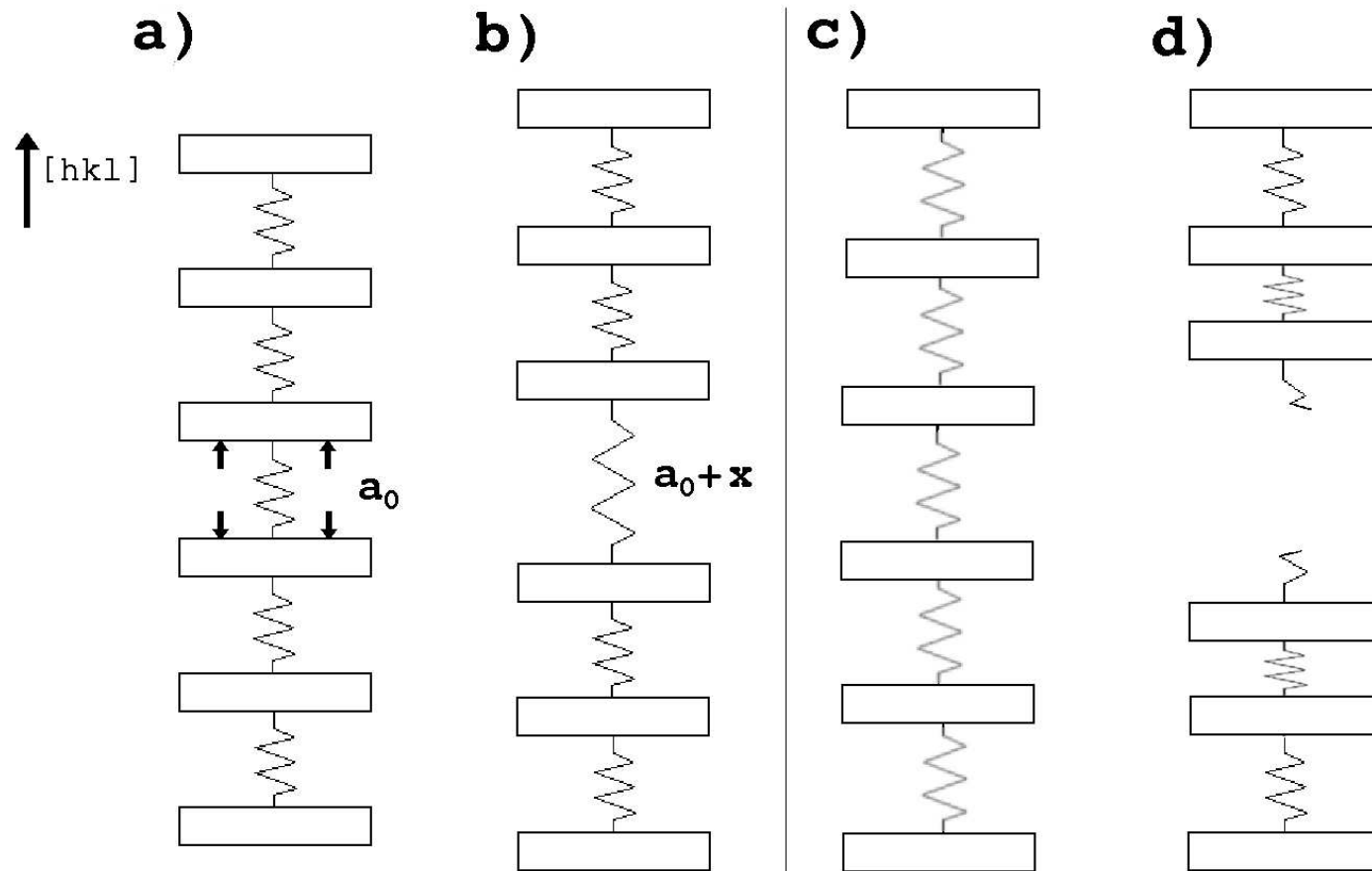
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<sup>1</sup>M. Polanyi, Z. Phys **7**, (1921)

<sup>2</sup>E. Orowan, Rep. Prog. Phys. **12** (1949)

<sup>3</sup>M. H. Yoo and C. L. Fu, Mat. Sci. Eng, **A153** (1992)

## Crack model:



For rigid block separation energy scales with  $x$  as (UBER)<sup>4</sup>

$$E_{DFT}(x) = G_b \left[ \left( 1 + \frac{x}{l_b} \right) \exp \left( -\frac{x}{l_b} \right) - 1 \right]$$

$G_b$  ..... cleavage energy

$l_b$  ..... critical length

The stress  $\sigma(x) = \frac{dE}{dx}$

Critical stress  $\sigma_b = \max \sigma(x) = \sigma(x = l_b)$

$$\sigma_b = \frac{1}{e} \frac{G_b}{l_b}$$

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<sup>4</sup>Rose et al. *Phys. Rev. B* **28** (1983)

Atoms are allowed to relax, initial crack closed until a relaxed value of cleavage energy  $G_e$  is reached.

At the critical point  $l_e$

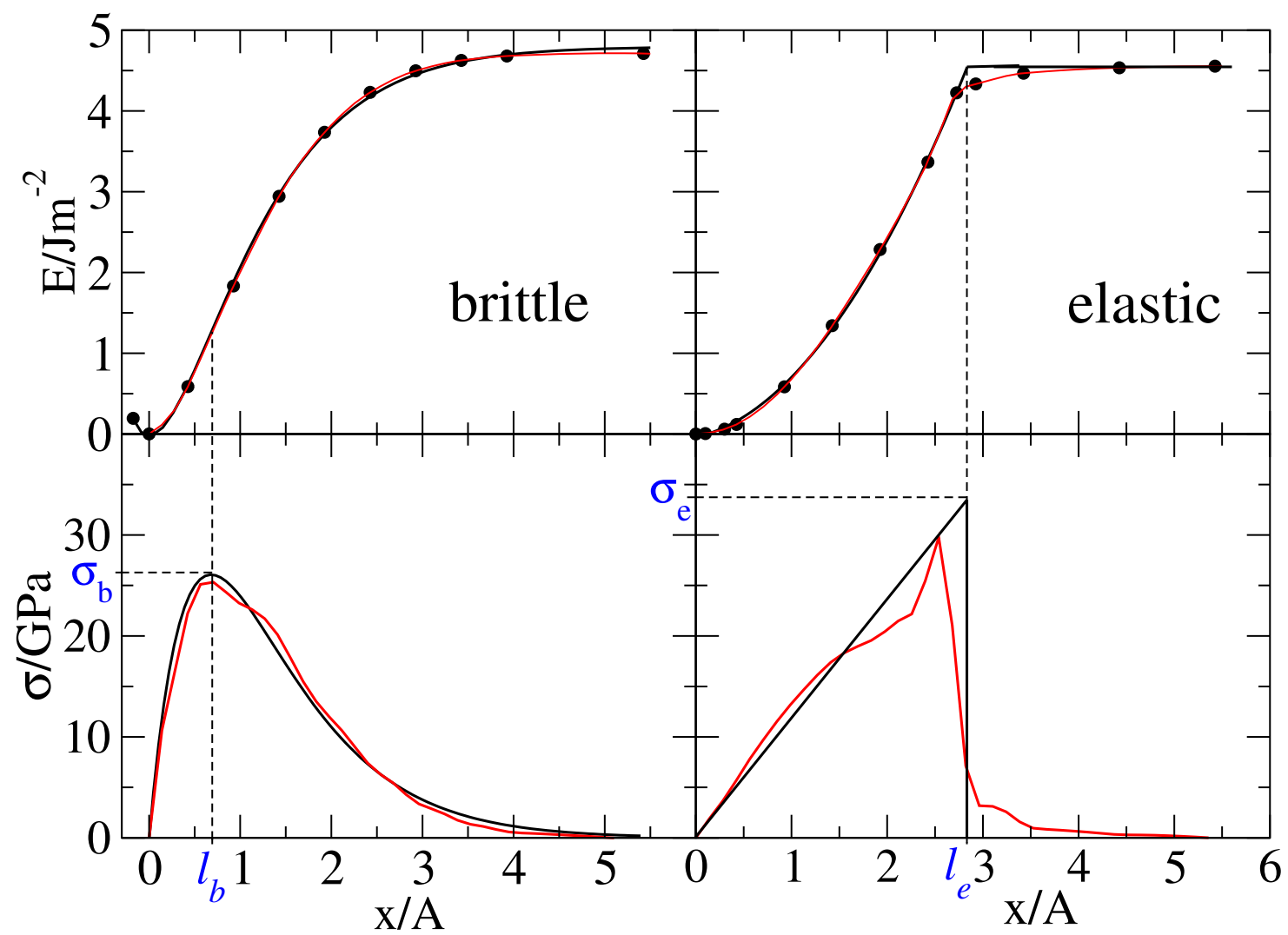
$$G_e = \frac{1}{2} A c_{11} \frac{l_e}{L}$$

Elastic energy

$$E(x) = \frac{G_e}{l_e^2} x^2$$

Maximum of the stress in the elastic limit

$$\sigma_e = 2 \frac{G_e}{l_e}.$$



## Connecting elasticity and fracture - key assumptions:

Assumption 1: at the critical limit  $x = l_b$  (the crack just forms) elastic energy and cleavage are at an unstable equilibrium, the elastic energy is localised in a local volume  $V = AL_b$ .

$$L_b = c_{11} \frac{l_b^2}{G_b}$$

As a fitting result:  $L_b$  is rather constant, independent of material and direction!!!

Assumption 2: at  $x \approx 0$ :

$$\frac{1}{2}AG_b \frac{x^2}{l_b^2} = \frac{1}{2}AL_b c_{11} \frac{x^2}{L_b^2}$$

Left side: Taylor expansion of UBER in lowest (second order) of  $x$ . Right side: elastic energy in volume  $V = AL_b$  described by elastic modulus  $c'_{11}$ <sup>5</sup>

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<sup>5</sup> $c'_{11}[hkl] = c_{11} - 2(c_{11} - c_{12} - 2c_{44})(h^2k^2 + k^2l^2 + l^2h^2)$



Stress:  $\sigma(x) = \frac{dE(x)}{dx}$

Critical stress:  $\max \sigma(x) = \sigma(x = l_b) = \frac{G_b}{el_b}$

With connection established:

$$\sigma_b = \frac{1}{e} \sqrt{\frac{G_b c_{11}}{L_b}}$$

Calculated values - **brittle limit**

		$l_b$	$L_b$	$l_e$	$L_e$
	$[hkl]$	$\text{\AA}$	$\text{\AA}$	$\text{\AA}$	$\text{\AA}$
NiAl	001	0.69	2.0	2.7	15.8
	011	0.54	2.5	2.0	17.7
	111	0.58	2.4	2.2	18.4
TiAl	001	0.82	2.6	3.0	17.5
VC	001	0.37	2.8	0.8	6.5
MgO	001	0.37	2.2	0.8	5.3
TiC	001	0.42	2.6	1.3	11.9

	$[hkl]$	$c'_{11}$ GPa	$G_b$ J/m <sup>2</sup>	$\sigma_b$ GPa	$G_e$ J/m <sup>2</sup>	$\sigma_e$ GPa
NiAl	001	203	4.8	26	4.6	34
	011	284	3.2	22	3.1	32
	111	327	4.1	26	3.9	36
TiAl	001	168	4.4	20	4.2	28
VC	001	647	3.2	32	2.4	60
MgO	001	299	1.8	18	1.7	42
TiC	001	515	3.5	31	3.2	50

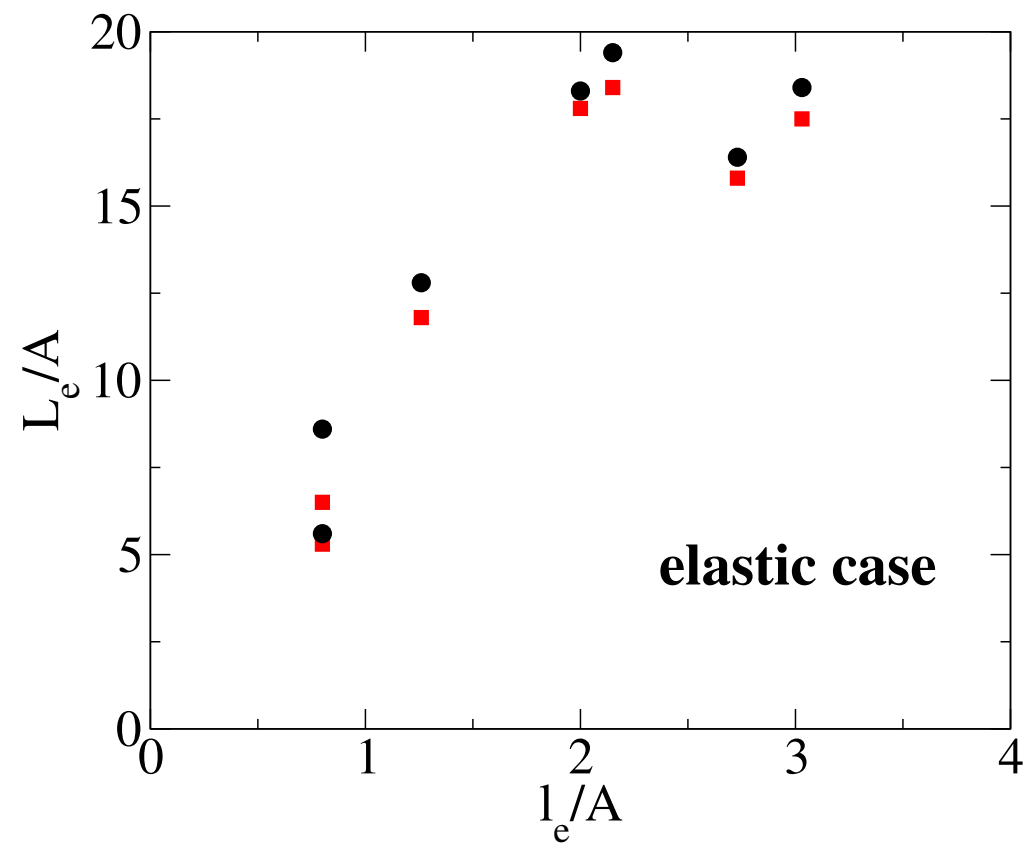
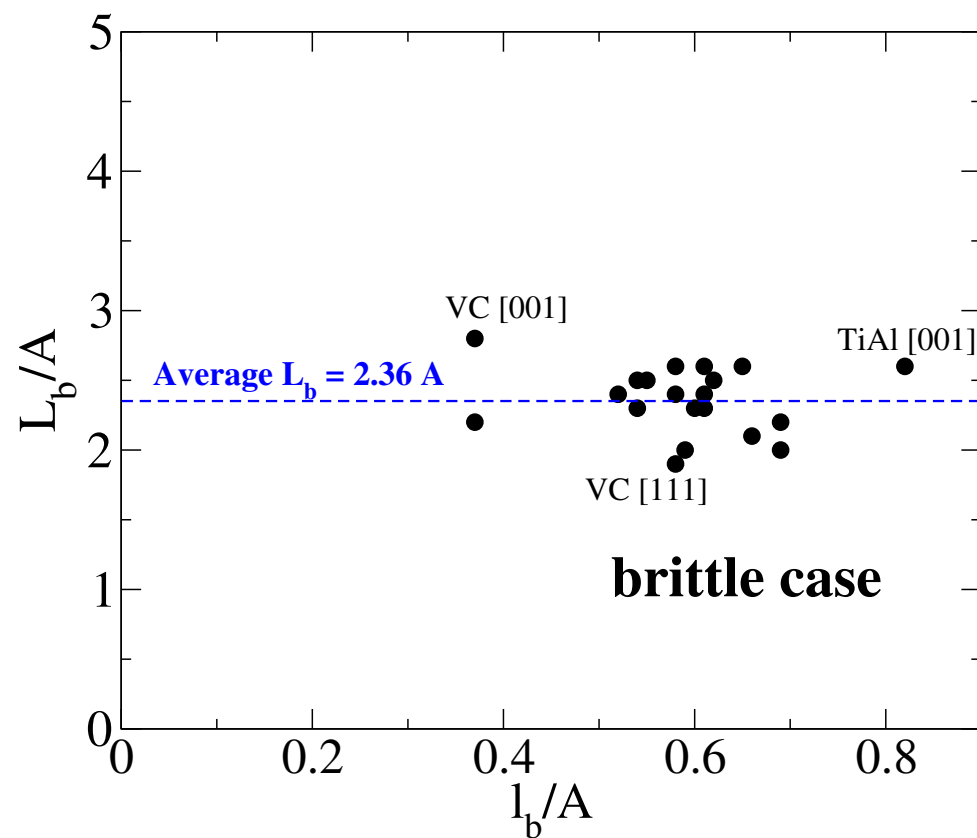
Calculated values - **brittle limit**

	direction [ <i>hkl</i> ]	$c'_{11}$ GPa	$G_b$ J/m <sup>2</sup>	$l_b$ Å	$\sigma_b$ GPa	$L_b$ Å
NiAl	001	203	4.8	0.69	26	<b>2.0</b>
	011	284	3.2	0.54	22	<b>2.5</b>
	111	327	4.1	0.58	26	<b>2.4</b>
TiAl	001	168	4.4	0.82	20	<b>2.6</b>
	111	262	3.5	0.58	22	<b>2.6</b>
VC	001	647	3.2	0.37	32	<b>2.8</b>
	011	585	7.0	0.55	46	<b>2.5</b>
	111	564	9.9	0.58	63	<b>1.9</b>
Fe	001	302	5.4	0.59	34	<b>2.0</b>
	111	350	5.8	0.61	35	<b>2.3</b>
MgO	001	299	1.8	0.37	18	<b>2.2</b>
	011	345	4.4	0.54	30	<b>2.3</b>

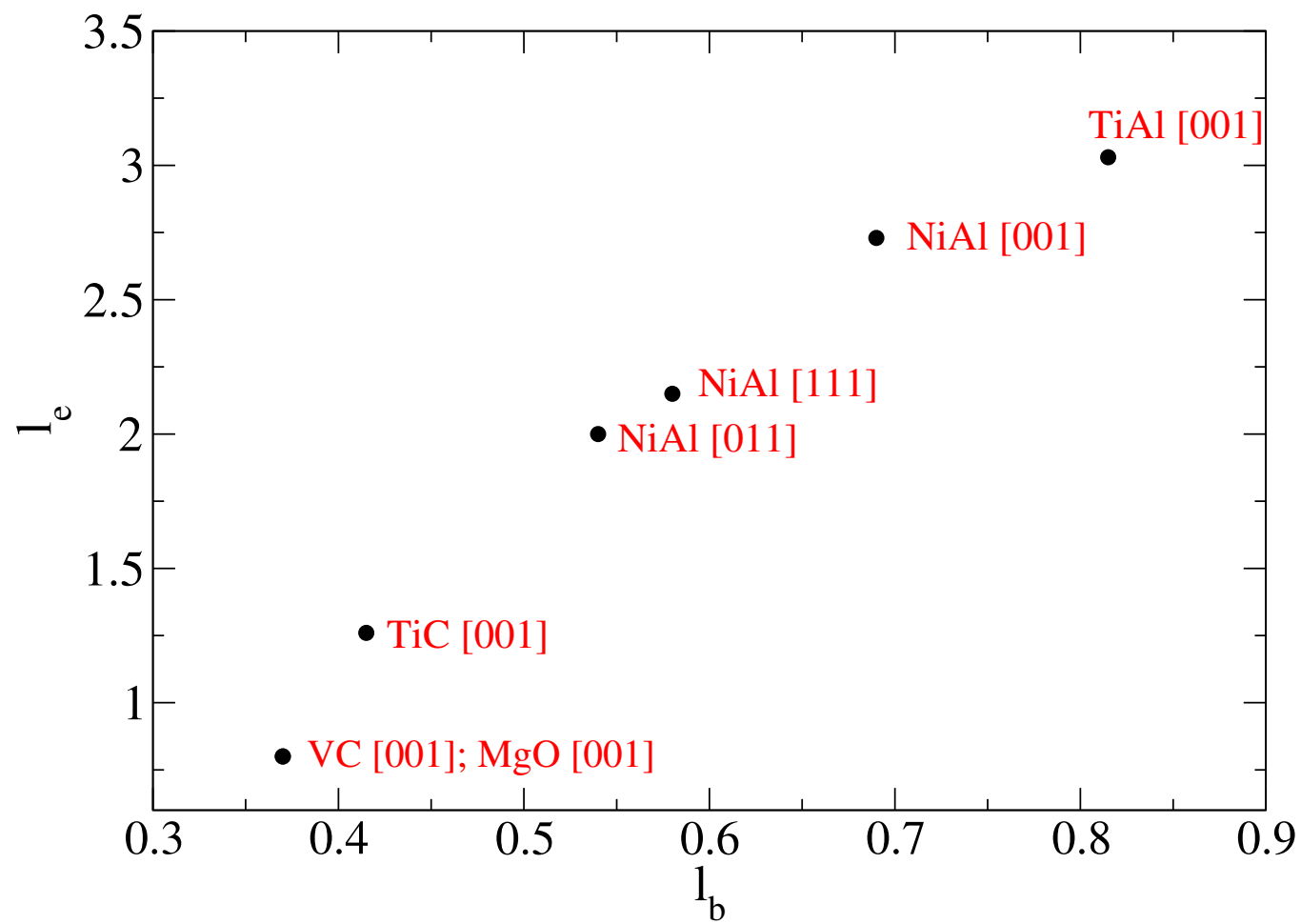
## Elastic limit

	direction [ <i>hkl</i> ]	$G_e$ (J/m <sup>2</sup> )	$l_e$ (Å)	$L_e$ (Å)	$\sigma_e$ (GPa)
NiAl	100	4.6	2.7	15.8	34
	110	3.1	2.0	17.7	32
	111	3.9	2.2	18.4	36
TiAl	001	4.2	3.0	17.5	28
MgO	001	1.7	0.8	5.3	42
VC	001	2.4	0.8	6.5	60
TiC	001	3.2	1.3	11.9	50

## Localisation lengths in both limits



## Correlation between critical lengths in both limits



## Conclusions

1. simple analytic formula for crack in the elastic limit was derived

$$E(x) = G_c \frac{x^2}{l_e^2}$$

2. using idea of localisation of the elastic energy just at the point of rupture of material a simple formula

$$\sigma_b = \frac{1}{e} \sqrt{\frac{G_b c_{11}}{L_b}}$$

for estimate maximum cleavage stress just via cleavage energy, elastic constant was obtained. A new parameter  $L_b$  - localisation length - was introduced.

3. localisation length in the brittle limit  $L_b$  was found rather material and direction independent in all cases inspected.



